



January 20, 2022 | Revision A

Marine Facility Condition Assessment of the Port Neville Wharf

Submitted to: Strathcona Regional District (SRD)
Prepared by McElhanney Ltd.

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1. Introduction

1.1. PROJECT BACKGROUND

McElhanney Ltd. (McElhanney) has been retained by the Strathcona Regional District (SRD) to complete a condition assessment of the marine facilities at the public wharf located in Port Neville, BC. Figure 1 shows the site location of the wharf.

The marine facilities are generally in moderate condition with assumed limited maintenance and inspection having been completed over the last 10 years. McElhanney's assessment will be used to determine the need for repairs and/or replacements.

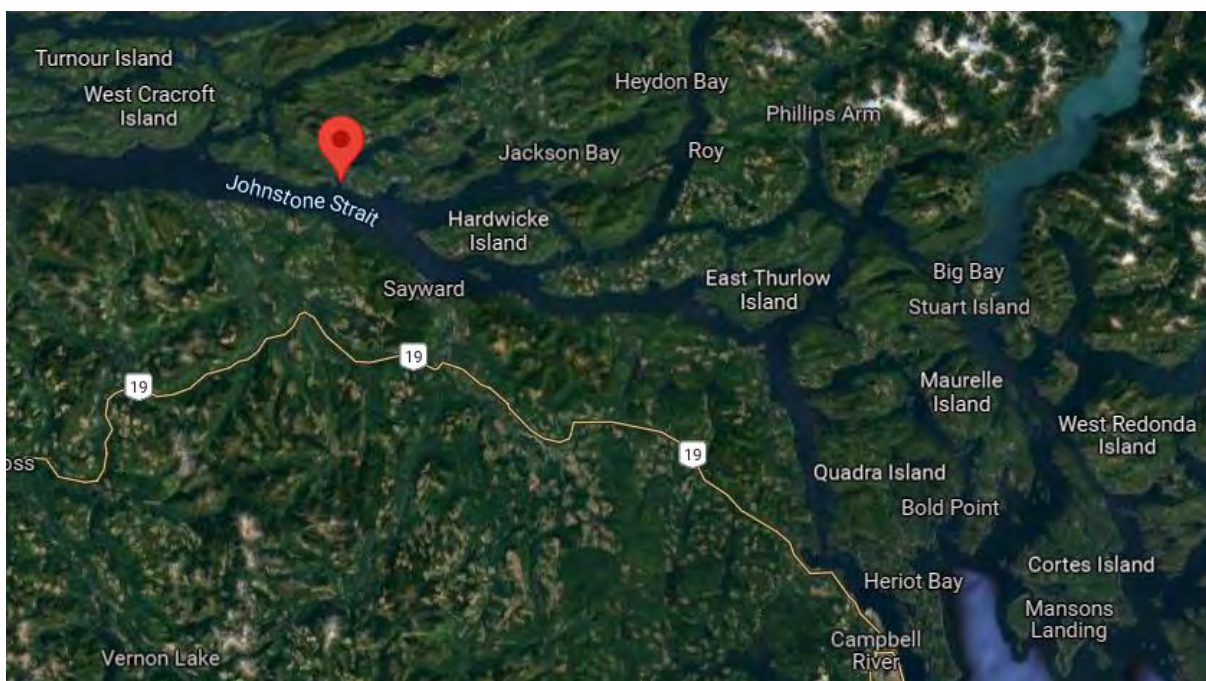


Figure 1 – Site Location

The visual site inspection, completed on September 1, 2021, and the coring inspection, completed on December 7th, 2021, was by the following McElhanney personnel:

- Hannah Hladkovicz, EIT, Marine Structural Engineer
- Zach Tillapaugh, EIT, Structural Engineer

1.2. REFERENCE DRAWINGS

The following reference drawings and documents are available and have been reviewed by McElhanney:

- Drawings 1-3: Port Neville, BC – Wharf and Float Repairs
- Port Divestiture Program – Final Report, January 2014
- Port Neville Location Map
- Transport Canada: Approach & Floats, Plan & Description Drawing
- Structure Condition Inspection and Report, Herold Engineering Ltd, February 2014.

1.3. REFERENCE SYSTEM

The reference system used in the inspection is consistent with Figure 2 below.

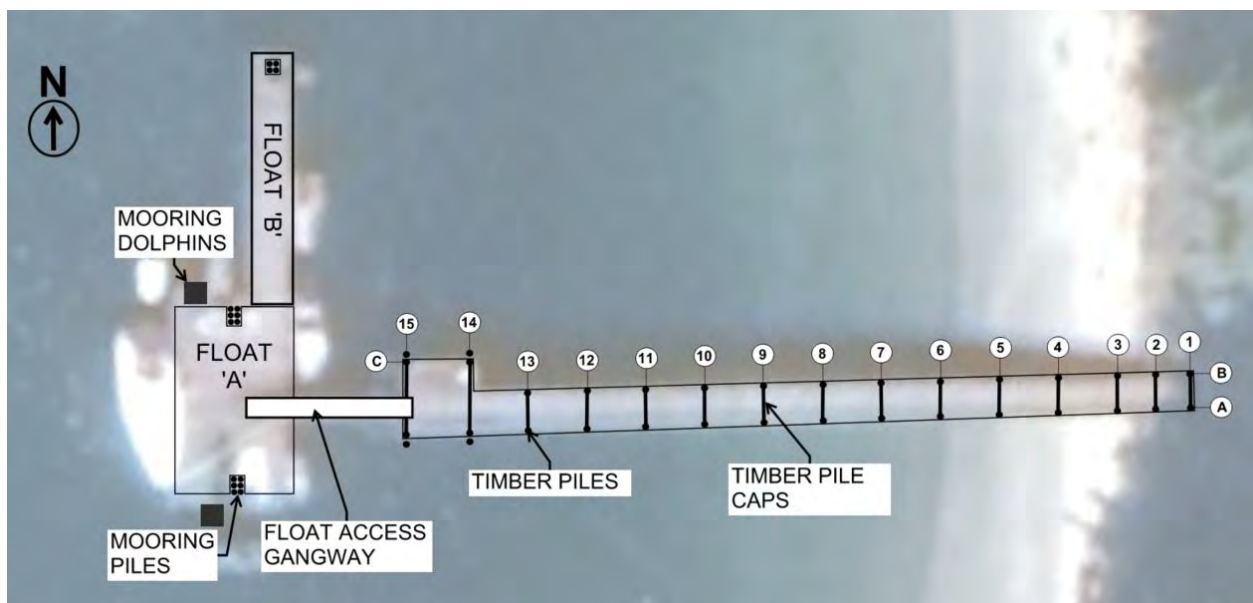


Figure 2 – Inspection Reference System

2. Description of Facilities

The wharf structure is a conventional treated timber wharf, approximately 60 meters long, and consisting of the following:

- Painted timber handrails including a top rail, mid-rail, and bull rail curb secured to handrail posts bolted to the edge stringer and bull rail
- Treated timber deck planks, typically 3" x 12"
- 6" x 12" stringers, typically at 30" centers
- 10" x 12" pile caps, typically at 15' centers
- 12" nominally sized creosoted treated piles at 8' centers along the bent. Bent Nos. 14 and 15 have (3) piles along the bent at the pierhead
- 12" fender piles at bents 14 and 15
- 12m long steel truss gangway
- The floating docks consist of treated timber decking and framing, and buoyancy billets.
- Float A has (12) mooring piles, (6) at the north end and (6) at the south end. There are two timber mooring dolphins, one at the north side of Float A, and one at the south side. Float B has 4 mooring piles at the north end.
- The North dolphin consists of 15 vertical timber piles and 4 batter piles, the South dolphin consists of 16 vertical piles. The mooring piles and dolphins are creosote coated timber piles.

Figures 3 and 4 provide reference sketches of the timber wharf approach trestle. Inspection photographs are provided in Appendix A.

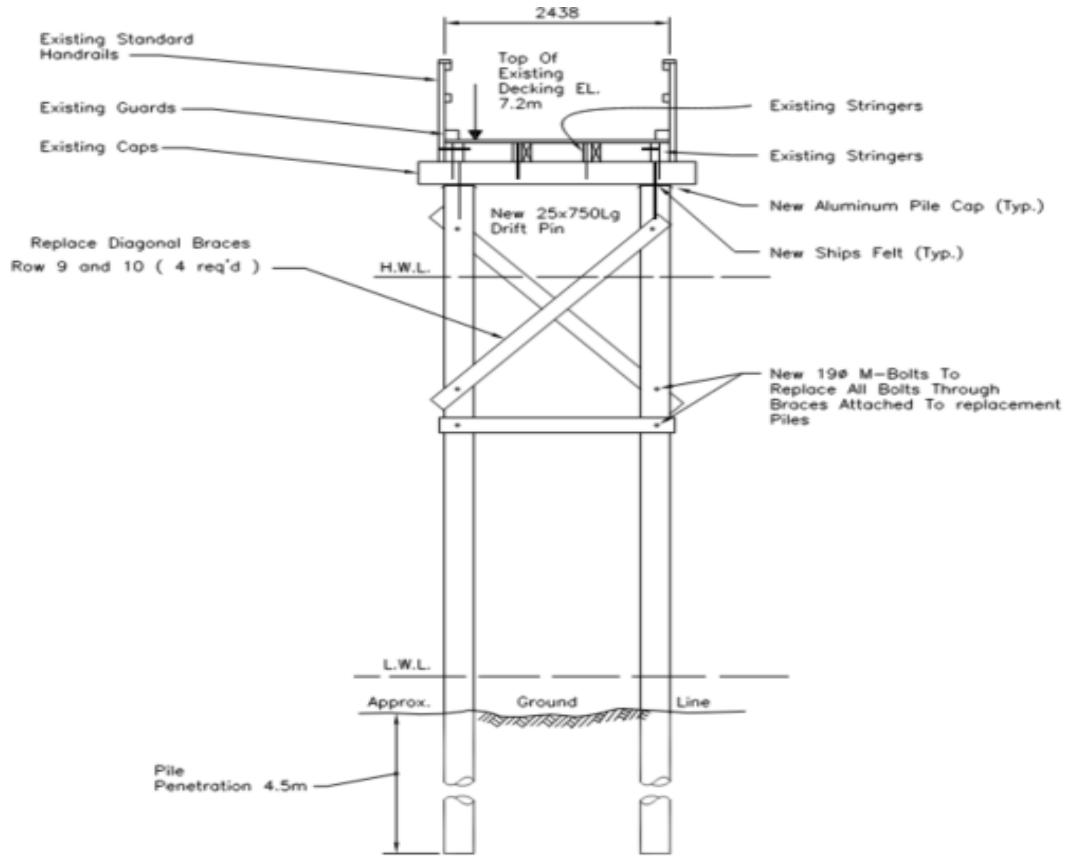


Figure 3 – Typical Structure Cross Section (Abutment to Bent No. 13)

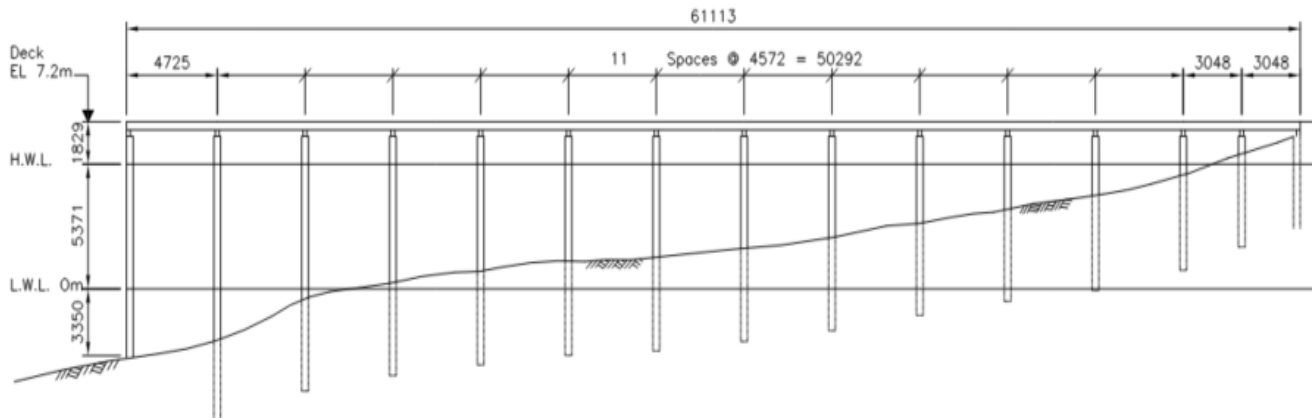


Figure 4 – Typical Structure Elevation

3. Inspection Methodology and Limitations

3.1. INSPECTION METHODOLOGY

An above water inspection of the marine assets was completed using visual inspections on September 1st, 2021, and timber coring on December 7th, 2021. The inspection methodology was completed in accordance with the procedures and recommendations provided in “Procedures for Inspection and Assessment of Fixed Timber Docks”, by RG Sexsmith Ltd. and dated September 1994, 4th Edition. This reference has been widely adopted by the Canadian Coast Guard, Department of Fisheries and Oceans Small Craft Harbours Branch, and Transport Canada in the evaluation and assessment of timber docks, piers, and wharves along the BC Coast.

The inspection methodology used is summarized as follows:

- Visual inspection of the timber elements from the lower intertidal zone to underside of deck was completed from land and from a small boat during a low tide window.
- An underwater inspection was completed to assess the condition of the piles. The inspection was completed using an underwater ROV mobilized from a small boat underneath the wharf structure.
- Timber coring was completed at the tops of the piles, pile caps, and stringers where steel drift pins are present, from bents 1-8. The timber coring is completed using a 13mm diameter drill which extends approximately 50% to 75% through the timber member. Fungal decay has significantly less resistance for the drill and so the resultant torque and drill cuttings from fungal decay are obvious to the inspector. From timber coring, the extent of fungal decay and cross-sectional loss (CSL) is expressed in intervals of 10%, 25%, 50%, 75%, and 90% CSL.

3.2. INSPECTION LIMITATIONS

The following inspection limitations should be considered when evaluating the results of the inspection findings:

- Both bankia and limnoria marine borers species are actively present on the BC Coast and can damage the timber pilings from the seabed to the intertidal zone. This should be identified during underwater inspections.
- The findings and recommendations are for the use of the SRD only.
- Users of the facility should always report any unusual conditions so that they can be evaluated by a Professional Engineer registered in British Columbia.

3.3. CONDITION

In accordance with the Ministry of Transportation and Infrastructure, Asset Performance Measures, for each structural element type, the overall condition state is provided based on a site inspection of each structure component.

- Excellent Condition – as-built condition, no observed defects.
- Good Condition – normal wear and deterioration
- Fair Condition – minor loss in condition or minor observed defects.
- Poor Condition – advanced loss in condition or significant defects.
- Very Poor Condition – serious loss in condition or serious defects.

4. Inspection Findings

4.1. PIER STRUCTURE

4.1.1. Approach

The pier approach is in generally good condition (Photos 1). There are no signs of settlement in this area, and the slope around the pier abutment appears stable. No load rating sign has been posted.

Repairs are not considered necessary at this time; however ongoing monitoring of the pier approach is recommended. Consideration should also be given to posting a load rating sign and extending safety barriers to the approach area.

4.1.2. Topsides and Decking

The pier topsides are generally in poor to fair condition with widespread weathering and fungal decay (Photos 2 & 3). Inspection findings are as follows:

- The handrails appear generally well secured. The handrail posts are connected to the pier structure with two bolts, one through the outer stringer, and one through the bull rail. In some locations, the bull rails are deteriorated or not fully secured, and the handrail posts can shift, however they are still well secured to the stringer. There is significant deterioration to multiple other top rail connections, the approximate locations are directly above the following piles:
 - Between piles 4B and 5B (Photo 4)
 - Between piles 7A and 8A (Photo 5)
 - Between piles 8B and 9B (Photo 6)
 - Between piles 9A and 10A (Photo 7)
 - Between piles 11A and 12A (Photo 8)
 - Between piles 12A and 13A (Photo 9)
- Identified during the second inspection on December 7th, 2021, the top rail connection directly above pile 14B has deteriorated and is only connected on one end (Photo 10). *It is recommended that the bull rails and handrail posts be fully replaced and secured in places with deterioration and/or missing bolts. Consideration should be given to painting the handrails to extend the service life of the existing timber. Consideration should also be given to a full phased replacement of the topsides over the next 2-4 years.*
- The timber deck planks have widespread minor weathering, however, are generally in good condition. All deck planks appear well secured. *Installation of an anti-slip grating to improve the safety during wet weather conditions is recommended. Continued monitoring of the condition of the topsides should be regularly completed.*

4.1.3.Stringers

The treated timber stringers are generally in good condition (Photo 11). The stringers appear well secured between the decking and the pile caps, and there are no signs of significant splitting or structural deterioration. The ends of the stringers, where the end grain is present, does not show significant evidence of moisture or fungal decay. No cross-sectional loss was found in the stringers during the timber coring inspection.

Repairs are not considered necessary at this time; however ongoing monitoring of the stringers is recommended.

4.1.4.Pile Caps

The treated timber pile caps are generally in fair to good condition (Photo 12 & 13). The pile caps appear well secured, and there are no signs of significant splitting or structural deterioration. The pile caps are typically aligned well over the piles, with no evidence of shifting or displacement. There is minor weathering and deterioration to the end grains of the pile caps, notably at Bent 12 (Photo 14). No cross-sectional loss was found in the pile caps during the timber coring inspection.

Repairs are not considered necessary at this time, however ongoing monitoring of the pile caps and of the deterioration at the end grains is recommended.

4.1.5.Piles

The structural timber piles are generally in fair to good condition, with some damage to isolated piles. Table 1 provides a location of specific timber pile findings.

Table 1 – Pile Inspection Findings

Location	Description	Recommendation
Pile 2A	Large split at the top of the pile. (Photo 15) 50% CSL due to internal fungal decay in the top 0.6m.	Replace timber pile.
Pile 2B	25% CSL due to internal fungal decay in the top 0.3m.	Monitor.
Pile 3A	25% CSL due to internal fungal decay in the top 0.3m.	Monitor.
Pile 3B	Moderate splitting at the top of the pile. (Photo 16) 25% to 75% CSL due to internal fungal decay in the top 0.9 m.	Replace timber pile.
Pile 4B	25% CSL due to internal fungal decay in the top 0.3m with wet fibres. Concrete footing is exposed, with signs of undermining and spalling of the concrete. (Photo 17)	Monitor.
Pile 5A	Moderate splitting at the base of the pile. (Photo 18)	Monitor.
Pile 5B	25-50% CSL due to internal fungal decay in the top 0.3m with wet fibres.	Replace timber pile.
Pile 7A	Pile is slightly misaligned. (Photo 19)	Monitor.

Pile 8A	Moderate splitting at the top of the pile. (Photo 20)	Monitor.
Pile 9A	Large open bolt hole at the top of the pile, likely from a previous cross-brace bolted connection. (Photo 21)	Monitor.
Pile 10A	Moderate splitting at the top of the pile. (Photo 22)	Monitor.
Pile 12A	Large open bolt hole at the top of the pile, likely from a previous cross-brace bolted connection. (Photo 23)	Monitor.
Pile 15B	Moss growing out of the top, indicating that there is fungal decay in the interior of the pile in this location. (Photo 24)	Monitor.

Repairs are not considered necessary at this time; however ongoing monitoring of the piles and areas of damage is recommended. It is anticipated that the piles identified with splitting and open holes will have established internal fungal decay in the next 5-10 years and should be considered for replacement.

4.1.6. Fendering System

The timber fender piles are generally in poor to fair condition, with one fender pile with severe fungal decay/marine borer cavities. Inspection findings are as follows:

- Fender Pile 10B has a marine borer cavity in the lower intertidal zone with 25% cross-sectional loss (CSL) (Photo 25).
- Fender pile 14A has a large marine borer cavity with 50% CSL, and likely severe cross section loss due to fungal decay (Photos 26 & 27). Marine growth appears to be coming out of the pile.
- Fender pile 15C has a large marine borer cavity with 50% CSL, and likely severe cross section loss due to fungal decay (Photo 28).

McElhanney understands that the fender piles are not longer used for vessel moorage and repairs are not considered necessary at this time as the fender piles are not structurally important to the pier.

4.1.7. Cross Bracing

The timber cross bracing is generally in fair to good condition (Photo 29 to 30). Inspection findings are as follows:

- There is widespread weathering, and minor fungal decay to the end grains of the members, however all cross braces appear well secured to the piles, apart from two locations.
- The cross bracing at Bent 8 appears to not be connected to pile 8A and is only resting on a timber block secured to the pile. (Photo 29)
- The cross bracing at Bent 15 is connected to the fender pile 15C, which has signs of significant cross-section loss. (Photo 30)

It is recommended that the cross braces at Bents 8 and 15 are re-secured. Ongoing monitoring of the cross bracing is recommended.

4.2. FLOATS

4.2.1. Access Gangway

The access gangway is in fair condition. The inspection findings are as follows:

- The upper hinge connection is slightly misaligned (Photos 31 and 32) which is likely to result in advanced wearing of the pinned connection.
- The timber gangway slider plate is in good condition with minor wearing and is well aligned with the gangway roller (Photo 33)
- The deck planks and anti-slip surface have moderate wearing (Photo 34).
- The steel truss members have typical minor to moderate coating failures and corrosion. No significant deterioration of the welded connections was noted (Photo 35).

McElhanney recommends that the access gangway be replaced in conjunction with future replacement of the floating docks.

4.2.2. Floats A and B

Float A is in poor to fair condition with minor deterioration to the topsides (Photo 36). Inspection findings are as follows:

- The timber deck planks have widespread moderate weathering and fungal decay, with localized deterioration. There is one location on Float B with plywood repair to the decking which is a tripping hazard (Photo 37)
- The floatation elements appear in fair condition.
- The west connection between Float A and Float B is rope (Photo 38). This is currently functioning properly, however this may be subject to rapid wearing and should be replaced with a steel chain in the future.
- The bull rails and fascia boards have widespread mechanical damage (Photo 39). The bull rail is missing in two locations.
- The east connection between Float A and Float B is chain which is causing moderate wearing to the floats (Photo 40).
- The mooring piles and mooring dolphins have moderate abrasion with the dock structures (Photo 41 to 33).

Consideration should be given to replacing Floats A and B along with the mooring system rather than continue regular minor maintenance/repairs.

4.2.3. Timber Mooring Dolphins

The timber mooring dolphins are in very poor condition. There is severe cross section loss due to internal fungal decay and marine borer cavity, as well as mechanical damage due to wearing of the floats.

Inspection findings are as follows:

- The north dolphin has vegetation growth near the tops of some of the piles. The timber blocking near the tops of the piles is deteriorating, and the cable wraps are loose (Photo 44)
- The south dolphin has significant vegetation growth near the tops of the piles. There is also severe cross section loss due to internal fungal decay and marine borer cavity in the intertidal zone, specifically on the front facing piles. The timber blocking is in poor condition, and the cable wraps are loose, but remain in place (Photo 45).

McElhanney understands that the mooring dolphins are no longer in service. To mitigate the risk of timber members contacting the dock, it is recommended that the timber dolphins be entirely removed and disposed of.

5. Residual Life Estimates

The marine facility is typically in fair condition. For the purpose of this evaluation, the residual life represents the estimated period of time between the inspection date and the time when the component will typically require repair or replacement.

For timber docks in a saltwater/marine environment, the residual life estimate is based on the follow:

- Where no established deterioration (marine borer cavities / fungal decay / mechanical abrasion) is noted in creosote treated timber, the remaining residual life is estimated to be 10+ years. As deterioration can progress rapidly in timber members once established, residual life estimates greater than 10 years are typically not given.
- Where deterioration has been established, the remaining residual life is estimated to be 2-7 years, depending on the extent of deterioration and likelihood to progress rapidly.
- Where there is deterioration which has significantly affected the structural capacity of the member the residual life is assumed to be minimal.

Based on McElhanney's understanding of the environment, usage, and familiarity with similar structures, Table 2 provides the estimates of the remaining service life of the wharf elements:

Table 2 - Summary of Recommendations

Location / Structure	Residual Life Estimate
Pier Structure	
Approach	+10 years
Topsides	1-2 years
Decking	5-7 years
Stringers	8-10 years
Pile Caps	5-7 years
Piles	5-7 years
Fender Piles	1-2 years
Floats	
Gangway	2-4 years
Float A	2-4 years
Float B	2-4 years
Mooring Dolphins	1< years

6. Facility Recommendations and Cost Estimates

The Port Neville Wharf facility is generally in fair condition and is expected to continue servicing public access for small craft vessels. Based on the inspection findings, there are a number of small maintenance items recommended. Table 2 provides recommendations and cost estimates based on McElhanney's understanding that the SRD intends to invest significant maintenance effort in the facility before 2024.

The cost estimates for the repairs are shown in Table 3.

Table 3 – Cost Estimates

Item	Priority	Description	Units	Quantity	Unit Cost	Subtotal
1	High	Install a load rating sign and approach barriers	LS	1	\$1,000	\$1,000
2	High	Repair and replace the handrails and bull rails where needed.	m	120	\$200	\$24,000
3	High	Phased replacement of the timber decking	m ²	150	\$250	\$37,500
6	High	Miscellaneous pile repairs/replacements (allowance)	Ea.	8	\$12,000	\$96,000
7	Medium	Replacement of the existing gangway.	m	15	\$2,000	\$30,000
8	Medium	Full Replacement of Float A and Float B	m ²	191	\$1,200	\$229,200
9	Medium	New steel mooring piles for Float A and B	Ea.	6	\$10,000	\$60,000
10	Medium	Remove and dispose of timber mooring dolphins.	LS	2	\$10,000	\$20,000
High Priority Subtotal						\$158,500
Contingency (25%)						\$39,625.0
High Priority Total						\$198,125
Medium Priority Subtotal						\$339,200
Contingency (25%)						\$84,800.0
Medium Priority Total						\$424,000
Total Capital Cost Estimate						\$622,125

In reviewing the cost estimates above, please note the following:

- The current vessel moorage capacity is sufficient for future use. No expansion or increase in vessel moorage capacity is anticipated.
- Estimated is based on available cost estimate material and labour rate data from recent projects between 2019 to 2021 and assumes competitive contractor pricing.
- Estimate is considered accurate to $\pm 50\%$. A contingency of 25% has been provided to account for cost items which have not been considered due to the extent of engineering work completed to date.

7. Closure

Please do not hesitate to contact the undersigned with any questions or comments.

Sincerely,
 McElhanney Ltd.
 Permit to Practice No. 1003299

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Revision History

Date	Status	Revision	Author
October 6, 2021	Draft Issue	A	M.Friderichs
January 20, 2022	For Use	0	M.Friderichs

Statement of Limitations

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inaccuracy contained in this report as a result of omissions or errors in information provided by third parties or for omissions, misstatements or fraudulent acts of persons interviewed.

Effect of Changes. All evaluations and conclusions stated in this report are based on facts, observations, site-specific details, legislation and regulations as they existed at the time of the site assessment/report preparation. Some conditions are subject to change over time and the Client recognizes that the passage of time, natural occurrences, and direct or indirect human intervention at or near the site may substantially alter such evaluations and conclusions. Construction activities can significantly alter soil, rock and other geologic conditions on the site. McElhanney should be requested to re-evaluate the conclusions of this report and to provide amendments as required prior to any reliance upon the information presented herein upon any of the following events: a) any changes (or possible changes) as to the site, purpose, or development plans upon which this report was based, b) any changes to applicable laws subsequent to the issuance of the report, c) new information is discovered in the future during site excavations, construction, building demolition or other activities, or d) additional subsurface assessments or testing conducted by others.

Independent Judgments. McElhanney will not be responsible for the independent conclusions, interpretations, interpolations and/or decisions of the Client, or others, who may come into possession of this report, or any part thereof. This restriction of liability includes decisions made to purchase, finance or sell land or with respect to public offerings for the sale of securities.

APPENDIX A – INSPECTION PHOTOS



Photo 1 – Pier Approach Area



Photo 2 – Pier Structure Topsides



Photo 3 – Pier Structure Handrails



Photo 4 – Handrail deterioration between piles 4B and 5B



Photo 5 – Handrail deterioration between piles 7A and 8A



Photo 6 – Handrail deterioration between piles 8B and 9B



Photo 7 – Handrail deterioration between piles 9A and 10A



Photo 8 – Handrail deterioration between piles 11A and 12A



Photo 9 – Handrail deterioration between piles 12A and 13A



Photo 10 – Handrail deterioration between piles 14B and 14C



Photo 11 – Typical View of Timber Stringers



Photo 12 – General View of Timber Pile Cap Bents



Photo 13 – Typical Timber Pile Cap End Grain



Photo 14 – Timber Pile Cap at Bent 12



Photo 15 – Split in Pile 2A



Photo 16 – Split in Pile 3B



Photo 17 – Pile 4B concrete footing



Photo 18 – Split in Pile 5A



Photo 19 – Pile 7A



Photo 20 – Split in Pile 8A



Photo 21 – Hole in Pile 9A



Photo 22 – Small split in Pile 10A



Photo 23 – Hole in Pile 12A



Photo 24 – Moss growth in Pile 15B



Photo 25 – Underwater image of damage to fender Pile 10B



Photo 26 – Fender Pile 14A



Photo 27 – Underwater image of marine borer cavity of fender pile 14A



Photo 28 – Fender Pile 15C

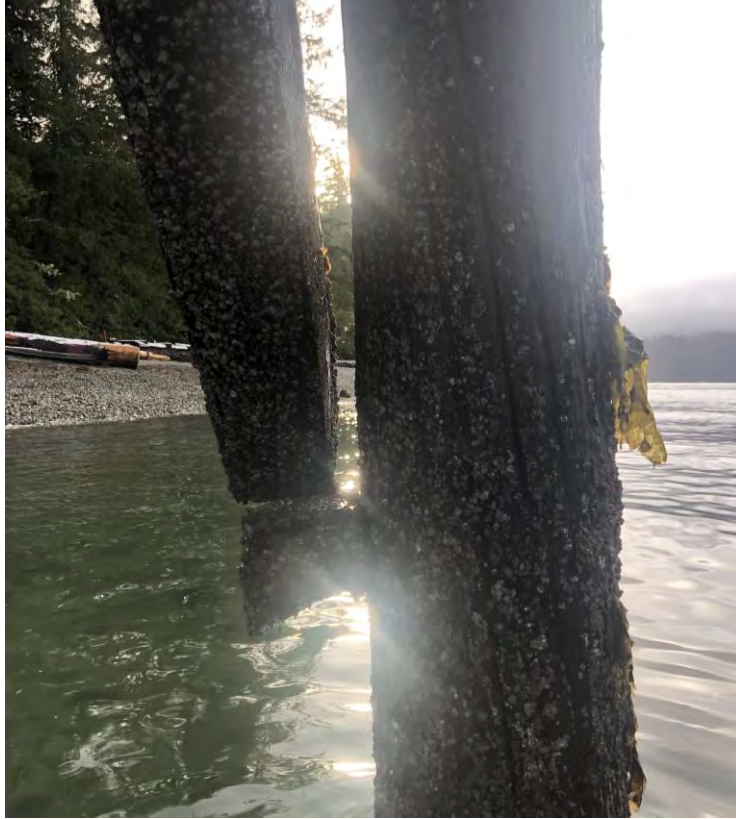


Photo 29 – Cross Bracing at Bent 8



Photo 30 – Cross Bracing at Bent 15



Photo 31 – Gangway Upper Hinge Connection



Photo 32 – Gangway Upper Hinge Connection



Photo 33 – Gangway Timber Slider Plate and Roller



Photo 34 – Gangway Timber Deck Planks



Photo 35 – Steel Gangway



Photo 36 – General view of Float A



Photo 37 – General view of Float B



Photo 38 – Rope connection to Float B



Photo 39 – Missing Bull rail on Float A



Photo 40 – Chain Connection to Float B



Photo 41 – Wearing to Float A from North Mooring Dolphin



Photo 42 – Wearing to Float A from South Mooring Piles



Photo 43 – Float A North Mooring Piles



Photo 44 – North Mooring Dolphin



Photo 45 – South Mooring Dolphin

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